



Whole-body Compliant Dynamical Contacts in Cognitive Humanoids

## WP5 related activities

**Francesco Nori**

francesco.nori@iit.it

Istituto Italiano di Tecnologia, Italy

April 16, 2015

Second year CoDyCo review meeting

Université Pierre et Marie Curie

Institut des Systèmes Intelligents et de Robotique

Paris, France

# WP5 Related Activities

A rough list

- ▶ From balancing towards walking WP3  
co-supervision of the intern Talha Arslan
- ▶ JTC for better tracking of desired link torques WP5  
supervision of the intern Raffaello Bonghi
- ▶ Calibration of force-torque sensors WP4  
working with Silvio Traversaro
- ▶ Adaptive control of underactuated systems WP4  
working with Francesco Romano
- ▶ Physical consistent inertial parameters on Lie groups WP4  
working with Silvio Traversaro

# WP5 Related Activities

A rough list

- ▶ From balancing towards walking WP3  
co-supervision of the intern Talha Arslan
- ▶ JTC for better tracking of desired link torques WP5  
supervision of the intern Raffaello Bonghi
- ▶ Calibration of force-torque sensors WP4  
working with Silvio Traversaro
- ▶ Adaptive control of underactuated systems WP4  
working with Francesco Romano
- ▶ Physical consistent inertial parameters on Lie groups WP4  
working with Silvio Traversaro

# WP5 Related Activities

A rough list

- ▶ From balancing towards walking WP3  
co-supervision of the intern Talha Arslan
- ▶ JTC for better tracking of desired link torques WP5  
supervision of the intern Raffaello Bonghi
- ▶ Calibration of force-torque sensors WP4  
working with Silvio Traversaro
- ▶ Adaptive control of underactuated systems WP4  
working with Francesco Romano
- ▶ Physical consistent inertial parameters on Lie groups WP4  
working with Silvio Traversaro

# WP5 Related Activities

A rough list

- ▶ From balancing towards walking WP3  
co-supervision of the intern Talha Arslan
- ▶ JTC for better tracking of desired link torques WP5  
supervision of the intern Raffaello Bonghi
- ▶ Calibration of force-torque sensors WP4  
working with Silvio Traversaro
- ▶ Adaptive control of underactuated systems WP4  
working with Francesco Romano
- ▶ Physical consistent inertial parameters on Lie groups WP4  
working with Silvio Traversaro

# WP5 Related Activities

A rough list

- ▶ From balancing towards walking WP3  
co-supervision of the intern Talha Arslan
- ▶ JTC for better tracking of desired link torques WP5  
supervision of the intern Raffaello Bonghi
- ▶ Calibration of force-torque sensors WP4  
working with Silvio Traversaro
- ▶ Adaptive control of underactuated systems WP4  
working with Francesco Romano
- ▶ Physical consistent inertial parameters on Lie groups WP4  
working with Silvio Traversaro

# WP5 Related Activities

A rough list

- ▶ From balancing towards walking WP3  
co-supervision of the intern Talha Arslan
- ▶ JTC for better tracking of desired link torques WP5  
supervision of the intern Raffaello Bonghi
- ▶ Calibration of force-torque sensors WP4  
working with Silvio Traversaro
- ▶ Adaptive control of underactuated systems WP4  
working with Francesco Romano
- ▶ Physical consistent inertial parameters on Lie groups WP4  
working with Silvio Traversaro

# Balancing

General definitions of the centroidal momentum

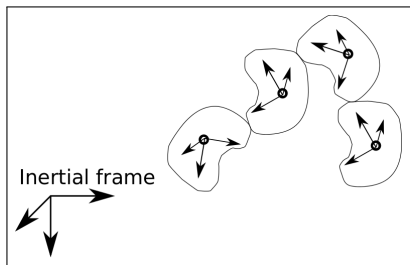
## Centroidal Momentum

$$M(q)\dot{v} + C(q, v)v + g(q) = \begin{bmatrix} 0 \\ \tau \end{bmatrix} + J_c^T f$$
$$J_c(q)\ddot{q} + \dot{J}_c\dot{q} = 0$$



# Balancing

General definitions of the centroidal momentum



- ▶  $\nu_i$  twist of the  $i$ th body
- ▶  $I_i$  : spatial inertia of the  $i$ th body

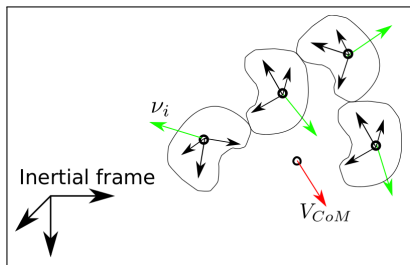
## Centroidal Momentum

$$H := \sum_{i=0}^n I_i \nu_i$$

$H$  is a coordinate-free (in the sense of Plucker) quantity

# Balancing

Centroidal momentum at the center of mass with inertial orientation



## Centroidal Momentum

$$H_{CoM} := \begin{pmatrix} m_{tot} V_{CoM} \\ f(q, \dot{q}) \end{pmatrix}$$

- ▶  $m_{tot}$ : total mass of the robot,  $q$ : joints' positions
- ▶  $V_{CoM}$ : velocity of the center of mass

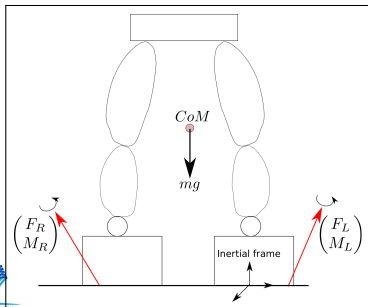
$$\frac{d}{dt} H_{CoM} = f_{Ext}^{CoM}$$

# Balancing

Control strategy when balancing on two feet

$$\dot{H}_{CoM} = \text{grav} + A(q)F_{\text{ext}}$$

$$M(q)\dot{v} + C(q, v)v + g(q) - J^T F_{\text{ext}} = \begin{pmatrix} 0_6 \\ \tau \end{pmatrix}$$

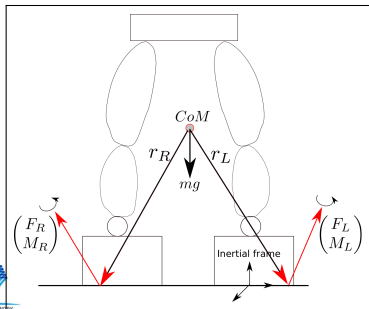


# Balancing

Control strategy when balancing on two feet

$$\dot{H}_{CoM} = \text{grav} + A(q)F_{\text{ext}}$$

$$M(q)\dot{v} + C(q, v)v + g(q) - J^T F_{\text{ext}} = \begin{pmatrix} 0_6 \\ \tau \end{pmatrix}$$



$$A(q) = \begin{pmatrix} I_3 & 0_3 & I_3 & 0_3 \\ r_L \times & I_3 & r_R \times & I_3 \end{pmatrix}$$

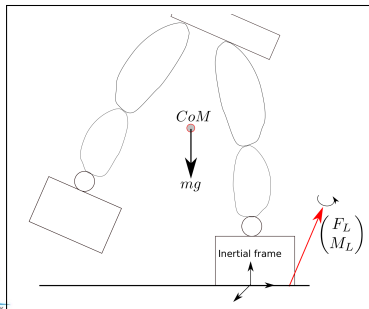
$$F_{\text{ext}} = \begin{pmatrix} F_L \\ M_L \\ F_R \\ M_R \end{pmatrix}$$

# Balancing

Control strategy when balancing on two feet

$$\dot{H}_{CoM} = \text{grav} + A(q)F_{\text{ext}}$$

$$M(q)\dot{v} + C(q, v)v + g(q) - J^T F_{\text{ext}} = \begin{pmatrix} 0_6 \\ \tau \end{pmatrix}$$



$$A(q) = \begin{pmatrix} I_3 & 0_3 \\ r_L \times & I_3 \end{pmatrix}$$

$$F_{\text{ext}} = \begin{pmatrix} F_L \\ M_L \end{pmatrix}$$

# Balancing

Control strategy when balancing on two feet

$$\dot{H}_{CoM} = \text{grav} + A(q)F_{\text{ext}}$$

$$M(q)\dot{v} + C(q, v)v + g(q) - J^T F_{\text{ext}} = \begin{pmatrix} 0_6 \\ \tau \end{pmatrix}$$

## Constraints on feet

$$J(q) := \begin{pmatrix} J_L \\ J_R \end{pmatrix}$$

$$J(q)\dot{v} + \dot{J}(q)v = 0$$

## Find $\tau$ such that

- (1)  $\dot{H}_{CoM} = \dot{H}_{CoM}^d, F_{Ext}^d \in FC$
- (2)  $q \approx q_d$  s.t.  $x(q_d) = x_d$

## Constraints on feet

$$J(q) := \begin{pmatrix} J_L \\ J_R \end{pmatrix} \rightarrow J(q) := \begin{pmatrix} I_n \alpha_l(t) & 0_n \\ 0_n & I_n \alpha_r(t) \end{pmatrix} \begin{pmatrix} J_L \\ J_R \end{pmatrix}$$

# Balancing

Control strategy when balancing on two feet

$$H_{CoM} = \begin{pmatrix} mV_{CoM} \\ H_w \end{pmatrix} \Rightarrow \dot{H}_{CoM} = \begin{pmatrix} m\dot{V}_{CoM} \\ \dot{H}_w \end{pmatrix} = \text{grav} + A(q)F_{ext}$$



# Balancing

Control strategy when balancing on two feet

$$H_{CoM} = \begin{pmatrix} m\dot{V}_{CoM} \\ H_w \end{pmatrix} \Rightarrow \dot{H}_{CoM} = \begin{pmatrix} m\ddot{V}_{CoM} \\ \dot{H}_w \end{pmatrix} = \text{grav} + A(q)F_{ext}$$

We choose  $F_{Ext}^d$  such that

$$\dot{H}_{CoM} = \dot{H}_{CoM}^d = \text{grav} + A(q)F_{ext}^d$$

We choose  $\dot{H}_{CoM}^d$  such that

$$x_{CoM} \rightarrow x_{CoM}^d \quad H_w \rightarrow 0$$

# Balancing

Control strategy when balancing on two feet

$$H_{CoM} = \begin{pmatrix} m\dot{V}_{CoM} \\ H_w \end{pmatrix} \Rightarrow \dot{H}_{CoM} = \begin{pmatrix} m\ddot{V}_{CoM} \\ \dot{H}_w \end{pmatrix} = \text{grav} + A(q)F_{ext}$$

We choose  $F_{Ext}^d$  such that

$$\dot{H}_{CoM} = \dot{H}_{CoM}^d = \text{grav} + A(q)F_{ext}^d$$

We choose  $\dot{H}_{CoM}^d$  such that

$$x_{CoM} \rightarrow x_{CoM}^d \quad H_w \rightarrow 0$$

A choice for  $F_{Ext}^d$  is

$$F_{ext}^d = A^\dagger(\dot{H}_{CoM}^d - \text{grav})$$

Pseudo-inverse suggests that there might be some null space to exploit (internal torques).

# Balancing

Control strategy when balancing on two feet

Given a desired CoM trajectory,  
we find the contact forces to stabilize it

# Balancing

Control strategy when balancing on two feet

Given a desired CoM trajectory,  
we find the contact forces to stabilize it

These contact forces lie in a 12-dimensional space, and are  
generated by the links' torques

# Balancing

Control strategy when balancing on two feet

Given a desired CoM trajectory,  
we find the contact forces to stabilize it

These contact forces lie in a 12-dimensional space, and are  
generated by the links' torques

The links' torques lie in a 25-dimensional space

# Balancing

Control strategy when balancing on two feet

Given a desired CoM trajectory,  
we find the contact forces to stabilize it

These contact forces lie in a 12-dimensional space, and are  
generated by the links' torques

The links' torques lie in a 25-dimensional space

How do we choose the remaining 13-dimensional space of  
the links' torques (inputs)?

# Balancing

Control strategy when balancing on two feet

$$\tau = \tau_f(F_{ext}^d) + N\tau_0$$

# Balancing

Control strategy when balancing on two feet

$$\tau = \tau_f(F_{ext}^d) + N\tau_0$$

$\tau_0$  is chosen as a proportional feedback (impedance behaviour around  $q_d$ ) plus gravity and external force compensation:

$$\tau_0 = g(q) + K_p(q - q_d) + J^T F_{ext}^d$$

$q_d$ , the postural configuration, is chosen to coincide with the solution of the Cartesian controller to perform goal directed actions with the hands and/or feet.



# Balancing

Control strategy when balancing on two feet

$$H_{CoM} = \begin{pmatrix} mV_{CoM} \\ H_w \end{pmatrix} \Rightarrow \dot{H}_{CoM} = \begin{pmatrix} m\dot{V}_{CoM} \\ \dot{H}_w \end{pmatrix} = \text{grav} + A(q)F_{ext}$$

A choice for  $F_{Ext}^d$  is

$$F_{ext} = A^\dagger(\dot{H}_{CoM}^d - \text{grav})$$

- ▶ No friction cones
- ▶ Even worse..

# Balancing

Control strategy when balancing on two feet

$$H_{CoM} = \begin{pmatrix} mV_{CoM} \\ H_w \end{pmatrix} \Rightarrow \dot{H}_{CoM} = \begin{pmatrix} m\dot{V}_{CoM} \\ \dot{H}_w \end{pmatrix} = \text{grav} + A(q)F_{ext}$$

A better choice for  $F_{Ext}^d$  is

$$F_{ext}^d = A^\dagger(\dot{H}_{CoM}^d - \text{grav}) + N_A F_0$$

Then, the torques are

$$\tau = \tau_f(F_0) + N\tau_0(F_0)$$

# Balancing

Control strategy when balancing on two feet

$$H_{CoM} = \begin{pmatrix} mV_{CoM} \\ H_w \end{pmatrix} \Rightarrow \dot{H}_{CoM} = \begin{pmatrix} m\dot{V}_{CoM} \\ \dot{H}_w \end{pmatrix} = \text{grav} + A(q)F_{ext}$$

A better choice for  $F_{Ext}^d$  is

$$F_{ext}^d = A^\dagger(\dot{H}_{CoM}^d - \text{grav}) + N_A F_0$$

Then, the torques are

$$\tau = \tau_f(F_0) + N\tau_0(F_0)$$

$$\tau_c = \arg \min_{F_0} |\tau(F_0)|$$

$$\text{s.t. } F_{ext}^d(F_0) \in FC$$

# Balancing

Conclusions, perspectives, and future work

- ▶ Smooth switching from double to single support
- ▶ Walking
- ▶ Implementation on the robot

# Publications

## Submitted papers

- ▶ "iCub Whole-body Control through Force Regulation on Rigid Noncoplanar Contacts" in *Frontiers in Robotics*
- ▶ "Collocated Adaptive Control of Underactuated Mechanical Systems" in *Transaction on Robotics*
- ▶ "In Situ Calibration of Six-Axes Force Torque Sensors using Accelerometer Measurements" in *ICRA*

# Balancing

Control strategy when balancing on two feet

$$\dot{H}_{CoM} = \text{grav} + A(q)F_{ext}$$

$$M(q)\dot{v} + C(q, v)v + g(q) - J^T F_{ext} = \begin{pmatrix} 0_6 \\ \tau \end{pmatrix}$$

## Constraints on feet

$$J(q) := \begin{pmatrix} J_L \\ J_R \end{pmatrix}$$

$$J(q)\dot{v} + \dot{J}(q)v = 0$$

# Balancing

Control strategy when balancing on two feet

$$\dot{H}_{CoM} = \text{grav} + A(q)F_{ext}$$

$$M(q)\dot{v} + C(q, v)v + g(q) - J^T F_{ext} = \begin{pmatrix} 0_6 \\ \tau \end{pmatrix}$$

## Constraints on feet

$$J(q) := \begin{pmatrix} J_L \\ J_R \end{pmatrix}$$

$$J(q)\dot{v} + \dot{J}(q)v = 0$$

# Balancing

Control strategy when balancing on two feet

$$\dot{H}_{CoM} = \text{grav} + A(q)F_{ext}$$

$$M(q)\dot{v} + C(q, v)v + g(q) - J^T F_{ext} = \begin{pmatrix} 0_6 \\ \tau \end{pmatrix}$$

## Constraints on feet

$$J(q) := \begin{pmatrix} J_L \\ J_R \end{pmatrix}$$

$$J(q)\dot{v} + \dot{J}(q)v = 0$$



# Balancing

Control strategy when balancing on two feet

$$\dot{H}_{CoM} = \text{grav} + A(q)F_{ext}$$

$$M(q)\dot{v} + C(q, v)v + g(q) - J^T F_{ext} = \begin{pmatrix} 0_6 \\ \tau \end{pmatrix}$$

## Constraints on feet

$$J(q) := \begin{pmatrix} J_L \\ J_R \end{pmatrix}$$

$$J(q)\dot{v} + j(q)v = 0$$

## Find $\tau$ such that

- (1)  $\dot{H}_{CoM} = \dot{H}_{CoM}^d, F_{Ext}^d \in FC$
- (2)  $q \approx q_d$  s.t.  $x(q_d) = x_d$